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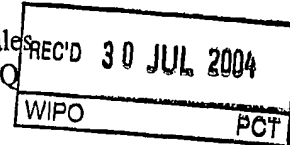
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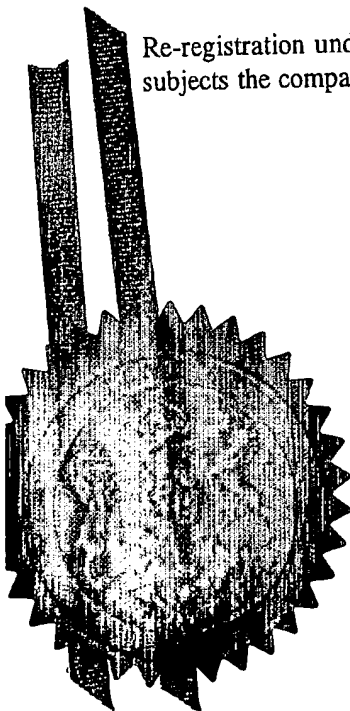
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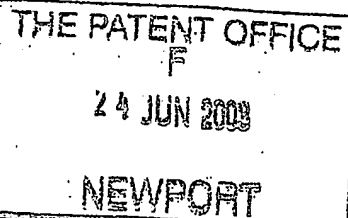
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*Andrew Gorse*

Dated 20 July 2004



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Request for grant of a patent

1. Your reference

TBS/BAR/37517.GBA

2. Patent application number

0314659 4

3. Full name, address and postcode of the or of each applicant (*underline all surnames*)

Anthony Bruce PIKE

12 4 JUN 2003

Patents ADP number

If the applicant is a corporate body, give the country/state of its incorporation

10 Auckland Close  
Upper Norwood  
LONDON

8659062001

SE19 2VN

4. Title of the invention

Medical Protection Sheeting

5. Name of your agent (*if you have one*)

Raworth Moss & Cook

"Address for service" in the United Kingdom to which all correspondence should be sent

36 Sydenham Road,  
Croydon, Surrey, CR0 2EF

Patents ADP number

1362001

6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or each of these earlier applications and (*if you know it*) the or each application number

Country Priority application number Date of filing

7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

8. Is a statement of inventorship and of right to grant of a patent required in support of this request? (*Answer yes if:*  
a) *any applicant named in part 3 is not an inventor, or*  
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Continuation sheets of this form 0

Description 7/

Claim(s) 0

Abstract 0

Drawing(s) 313

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Translations of priority documents 0

Statement of inventorship and right to grant of a patent (*Patents Form 7/77*) 0

Request for preliminary examination and search (*Patents Form 9/77*) 0

Request for substantive examination (*Patents Form 10/77*) 0

Any other documents (*please specify*) 0

11.

I/We request the grant of a patent on the basis of this application  
Signature

Date

*Laurie M. Smith*

23 June, 2003

12. Name and daytime telephone number of person to contact in the United Kingdom

Mr T Bain Smith  
020 8688 8318

### MEDICAL PROTECTION SHEETING

5 The present invention relates to medical protection sheeting  
useful for patient handling and designed to reduce the risk  
of damage to the skin of patients where this is damaged or  
where it is subject to pressure.

10 Patient handling sheeting is known for turning patients or  
lifting them between beds and trolleys and are sometimes  
known as "slide sheets", a term which will be used below.  
Where patients are severely injured, the movement between  
beds and trolleys can be difficult with known slide sheets  
15 since the material used for slide sheets is such as to cause  
high initial resistance to sliding, that is, the coefficient  
of friction rapidly rises as the sheet is pulled, reaching a  
peak before sliding actually commences. The sheet then, so  
to speak, becomes "unstuck". This sudden release from a  
high frictional resistance is the frequent cause of damage  
20 to a patient's skin, particularly where this has been burnt  
or in other cases where the epidermis is damaged. In some  
cases, this can cause separation of the dermal-epidermal  
junction.

25 Even where the epidermis is not initially damaged, decubitus  
ulcers or bedsores can form due to reduced blood flow in a  
local area of skin slowing because of pressure. By  
frequently changing body positions, this problem can be  
solved.

30 Further problems occur with dressings which rub on bedding  
or clothing. Again, high frictional coefficient between the  
dressing and material with which it is in contact can cause  
rucking of dressings and again epidermal damage.

35 According to the invention, there is provided medical  
protection sheeting formed from a low frictional material

having a coefficient of static friction substantially the same as its coefficient of dynamic friction.

5 The advantage of such a material is that as the material just starts to move over an adjacent material, which where possible is the same material, there is a smooth and gentle initiation and acceleration with no jerking. Thus epidermal damage is limited. Where slide sheets are made of the material of the invention, there is also less energy  
10 required by those caring for the patient. Where there is a concern for bedsores, then the patient may himself be able to move alternatively and again less energy may be used by carers to frequently move the patient lying on the material.

15 Preferred materials have a coefficient of friction less than 0.4.

Preferably the material is a woven fabric to enable a certain amount of "breathing". The material should not be  
20 too coarse and it is considered that materials having a linear density of 1000 to 40 decitex should be satisfactory.

Materials of 470, 350 and 50 decitex have been tried and perform well. The materials weigh respectively for the 350 and 50 decitex material 180 and 61.7 gm/m<sup>2</sup>. The finest  
25 material used which performed well under test was DuPont Tactel (RTM) having nylon warp yarn 50F15T143 and nylon weft yarn 50F15T1943. A coarser fabric identified as 470T743 has been used with success. A medium weight fabric identified as DuPont's 350T749 was successfully used.

30

Embodiments of the invention will now be described by way of example with reference to the accompanying drawings and diagrams in which:-

35 Figure 1 is a diagram of a test rig to test materials for the invention;

Figure 2 shows test results from the rig of Figure 1 to compare material according to the invention with linen so as to indicate relative coefficients of friction;

5 Figure 3 is an extract from the results of Figure 2;

Figure 4 is a set of test results from the rig of Figure 1 showing how varying the relative orientation between samples of the same material according to the invention varies the friction between the samples; and  
10

Figure 5 shows a bootee made with material according to the invention.

15 Samples of DuPont (DTI) plain woven nylon fabric from which slide sheets and dressing covering were made and were tried out as follows:-

Parafricta (TM) Ref	DTI Ref	Linear Density (decitex)	Weight g/m <sup>2</sup>	Gauge mm	Finished Threads per cm	Tensile Strength kN
P470	470T743	470		0.4	24 x 20	
P350	350T749	350	180	<0.35		>2.3
P50	98Wext/4	50	61.7	0.15	61x47	6*

20

\*Shear strength kN/m<sup>2</sup>

Samples of P470 fabric were submitted to the test rig shown in Figure 1 for the purpose of comparing its performance with linen on a linen to linen basis, P470 to P470, P470 to  
25 linen and linen to P470.

A block on flat measurement technique was used (Figure 1). A 50 x 50 mm sledge S wrapped in test fabric T1 was pulled  
30 over a flat plate F which was covered by a sheet of the second fabric T2 to be tested. The sledge was pulled at a

constant speed of 1 mm per second using a steel wire and a pulley by an Instron mechanical testing system LC. The load that was needed to pull the sledge gives the friction load and was recorded throughout the test. The sledge was loaded by weights giving a 40 N vertical load during the test. The friction coefficient is calculated as the frictional force divided by the applied load.

The results are shown schematically in Figure 2, with the main features given in Table 1. The highest friction values were recorded for the linen rubbing against linen where the static friction coefficient was 0.67 and the dynamic friction coefficient was 0.44. By contrast the static friction coefficient and dynamic friction coefficient were about 0.2 for the P470 rubbing on itself. When P470 was rubbing on linen, or linen on P470, the results were very similar with a dynamic friction coefficient of about 0.3 with a slightly higher static friction coefficient. Figure 3 extracted from Figure 2 shows that static friction increases rapidly from the application of a load until linen stretches. The linen then suddenly starts to slide, at which point the dynamic friction decreases rapidly.

Table 1, Main Results

Figure 2 Trace	Sledge Fabric (T1)	Flat Fabric (T2)	Static Friction	Dynamic Friction
12	Linen	Linen	0.67	0.44
11	P470	P470	0.19	0.21
13	P470	Linen	0.38	0.33
14	Linen	P470	0.33	0.29

Having completed the comparative tests of P470 against linen, a second series of tests was conducted to determine the effect of relative orientation as between warp and weft

of P470 material. The same rig (Figure 1) was used as in the first series of tests.

In the first set of the second series of tests, the load was recorded by chart recorder and then scanned and digitised to obtain digital results. For the second set of measurements, the load was recorded directly by a data logging system in a digital form.

The results are shown schematically in Figure 4, with the main features given in Table 2. The highest friction values were recorded for the linen rubbing against linen where the static friction coefficient was 0.67 and the dynamic friction coefficient was 0.44. By contrast, the static friction coefficient and dynamic friction coefficient were about 0.2 for the P470 rubbing on itself. When P470 was rubbing on linen, or linen on P470, the results were very similar, with a dynamic friction coefficient of about 0.3 with a slightly higher static friction coefficient. There was very little difference between the friction results for all the P470 on P470 tests.

The uncertainty of measurements of this type has not been studied definitively, but general experience of friction measurements would suggest that at an average friction level of about 0.2, the uncertainty in friction coefficient measurement is about 0.03.

Table 2, Further Results. Across is the direction on the P470 fabric parallel to the weft on the sample supplied. Along is perpendicular to this and parallel to the warp.

Figure 4 Trace	Sledge Fabric T1	Flat Fabric T2	Static Friction	Dynamic Friction
	Linen	Linen	0.67	0.44
24	P470 - Along	P470 - Along	0.19	0.21



	P470 - Along	Linen	0.38	0.33
	Linen	P470 - Along	0.33	0.29
21	P470 - Along	P470 - Across	0.24	0.24
22	P470 - Diagonal	P470 - Across	0.21	0.21
23	P470 - Across	P470 - Across	0.23	0.23

Trace 21 marked "crossed" on Figure 4 indicates the Sledge  
and Flat fabrics are orientated warp to weft or  
Along/Across.

The comparative second series of tests showed that the P470  
material was best aligned to another sample of itself so  
that both the warp threads were parallel, that the movable  
sheet was pulled in the warp direction and remarkably that  
the static friction was slightly less than the dynamic  
friction. The most unfavourable relative orientation was  
when the P470 materials were warp to weft or "crossed".  
However, as long as P470 was arranged to slide on P470,  
there was no great difference in the coefficient of friction  
for any relative orientation. In none of the relative  
orientations was there any great difference and most had the  
same static and dynamic coefficient of friction. This  
showed that unlike the linen on linen case shown in Figure  
3, there was no tendency for sudden jerking when using P470  
to P470 in juxtaposition. Sudden jerking would result in  
sudden uncontrolled motion.

Although it is desirable to use P470 to P470, the results of  
the tests of P470 to linen show that this is considerably  
better than using linen to linen. Furthermore, when using  
P470 to linen, it is best to pull the P470 in the warp

direction when on linen. It is therefore preferable when making a slip sheet (often about 120 x 70 cm or 145 x 72 cm) to cut the material so that the long side of the sheet runs parallel with the weft. Obviously, a range of sizes may be supplied up to about 200 cm long and up to 100 cm wide.

It will be observed that when using the material of the invention as a slide sheet, the force  $F$  to pull the sheet under a patient of weight  $W$ , the force required where  $\mu$  is the coefficient of friction and  $g$  is the acceleration due to gravity, that  $F = 2\mu gW$ , where static  $\mu$  ( $\mu_s$ ) is much greater than dynamic  $\mu_d$ , then  $F$  is increasingly greater to start moving the patient. Generally it can be shown that the material of the invention requires only about half the effort ( $F$ ) when compared to a sliding linen over linen. Also, the material can be made strong for any given weight of material.

Generally,  $\mu_s$  should be no more than 20% greater than  $\mu_d$  and both should be less than 0.4.

When using the material of the invention as a covering for a dressing, for example, as shown in Figure 5 which is in the form of a bootie 30 with a Lycra (RTM) collar 32, adjustable Velcro (RTM) closers 33 and externally seamed 34, a finer material such as P50 is preferred. Other forms (not shown) of covering for dressings are provided but which are also shaped to other particular parts of the body.

A particular application of the covering according to the invention is to protect dressings comprising advanced materials such as hydrocolloids which could include active materials to protect against infection or promote healing. Although these dressings may be more expensive than conventional dressings, the protection given by the covering of the invention enables these advanced dressings to remain in place longer. Therefore cost savings ensue.

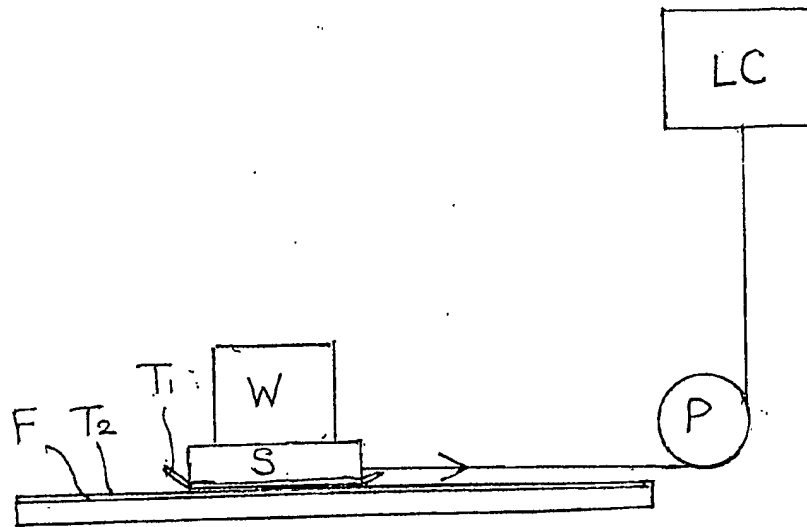


Figure 1

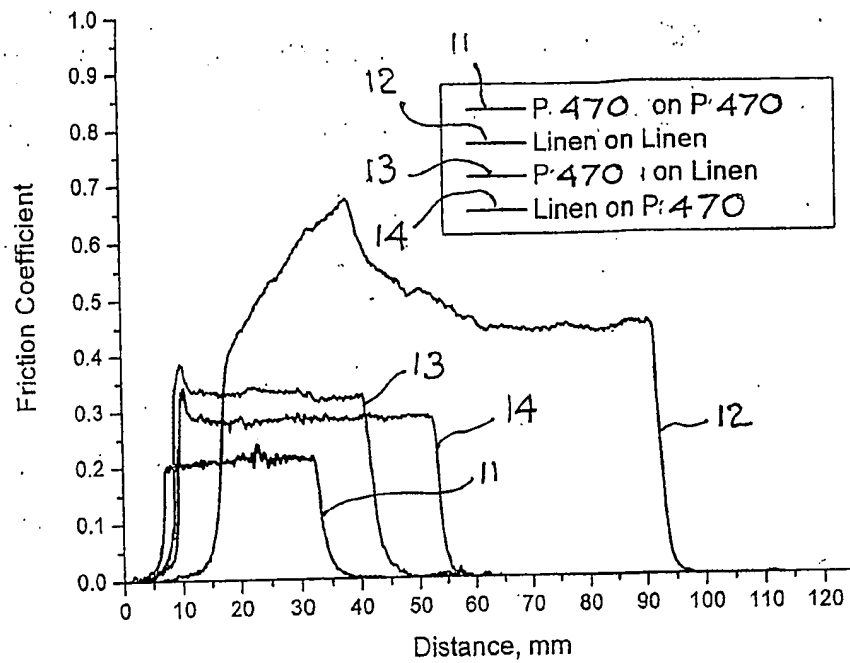


Figure 2, Variation in friction coefficient with sliding distance

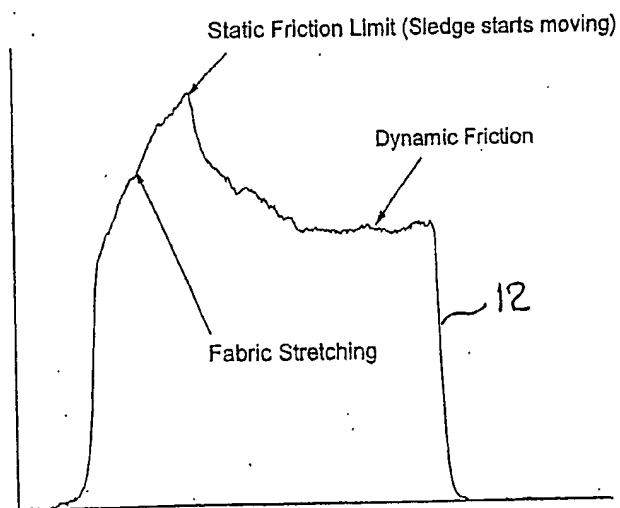


Figure 3, Illustration of static and dynamic friction using linen on linen results as an example.

Figure 4.

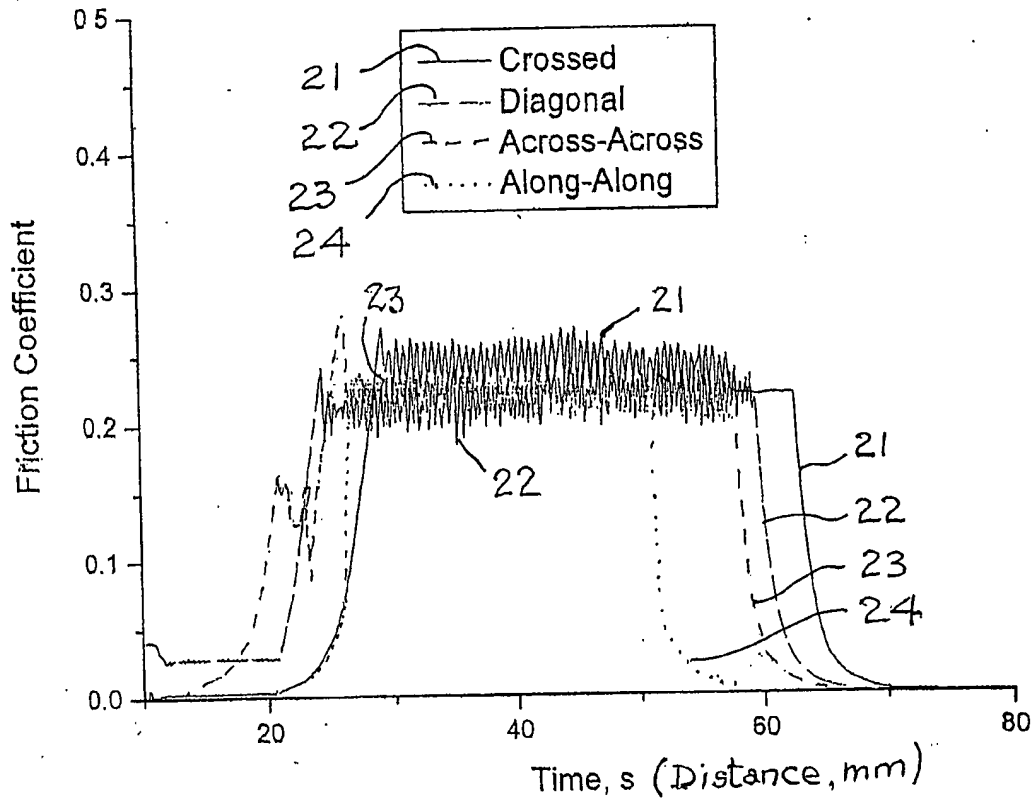
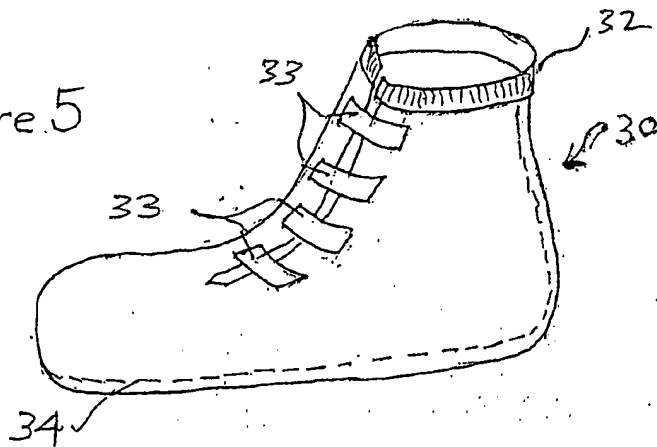


Figure 5



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